

Hull girder failure under combined global and local loads

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Subject of the thesis

1. FE progressive collapse analysis of bulk carrier and of container ship
2. Comparison with Poseidon software that uses Smith's method
3. Influence of the local loads

Capesize bulk carrier

$L_{pp} = 280,8 \text{ m}$ app. 170 000 dtw

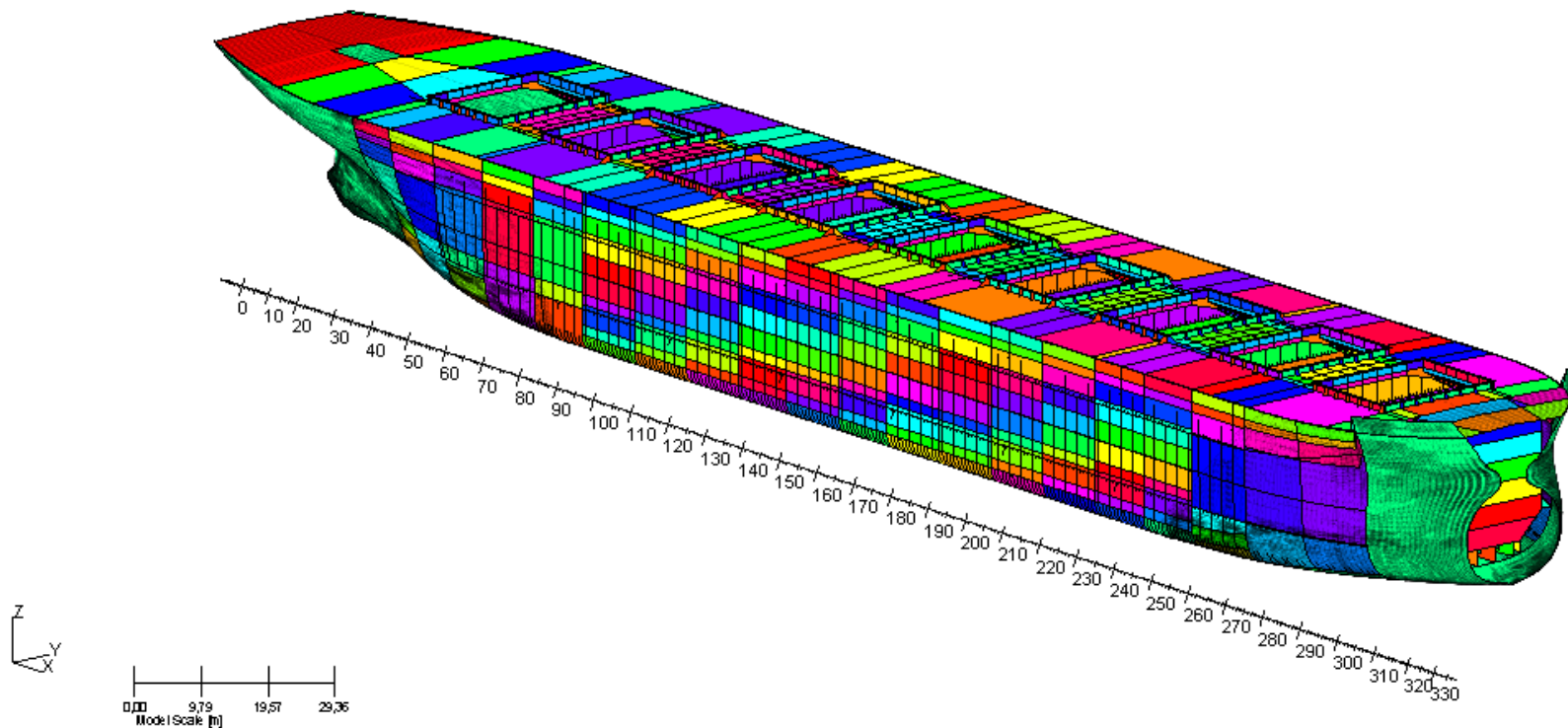


Fig. 1 Example of the bulk carrier model given in the GL - Poseidon

$L_{pp} = 349,5 \text{ m}$ app. 14 000 teu

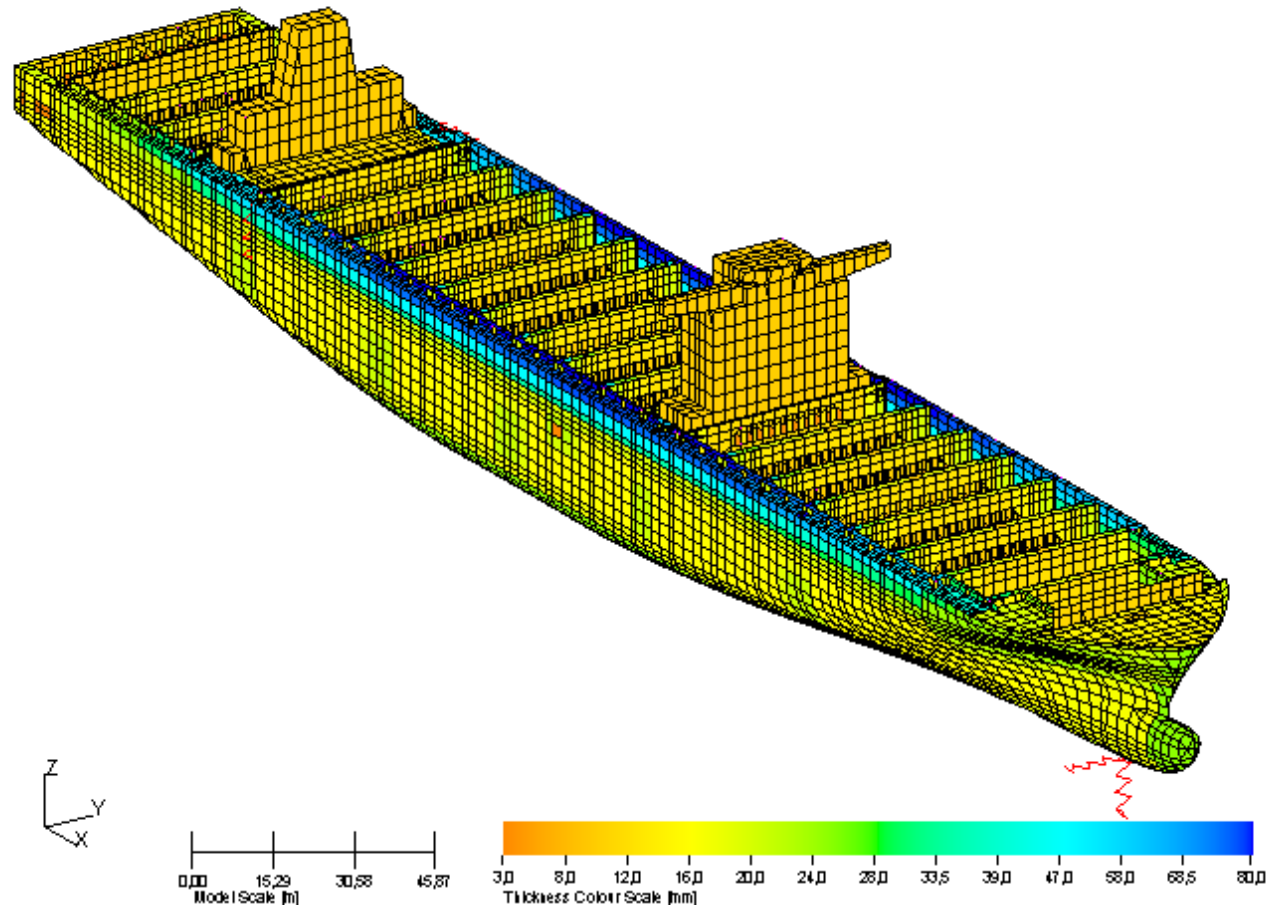


Fig. 2 Example of the container ship model given in the GL - Poseidon

Progressive collapse

1. Applying curvature
2. Calculating strain in the elements
3. Calculating stresses
4. Change of the neutral axis
5. Moment acting
6. If μ not reached repeat the steps with increased curvature

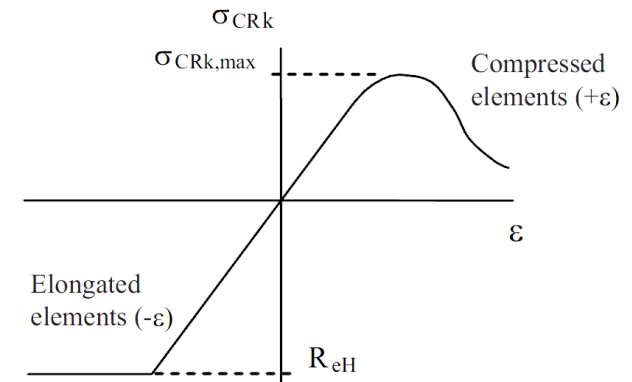
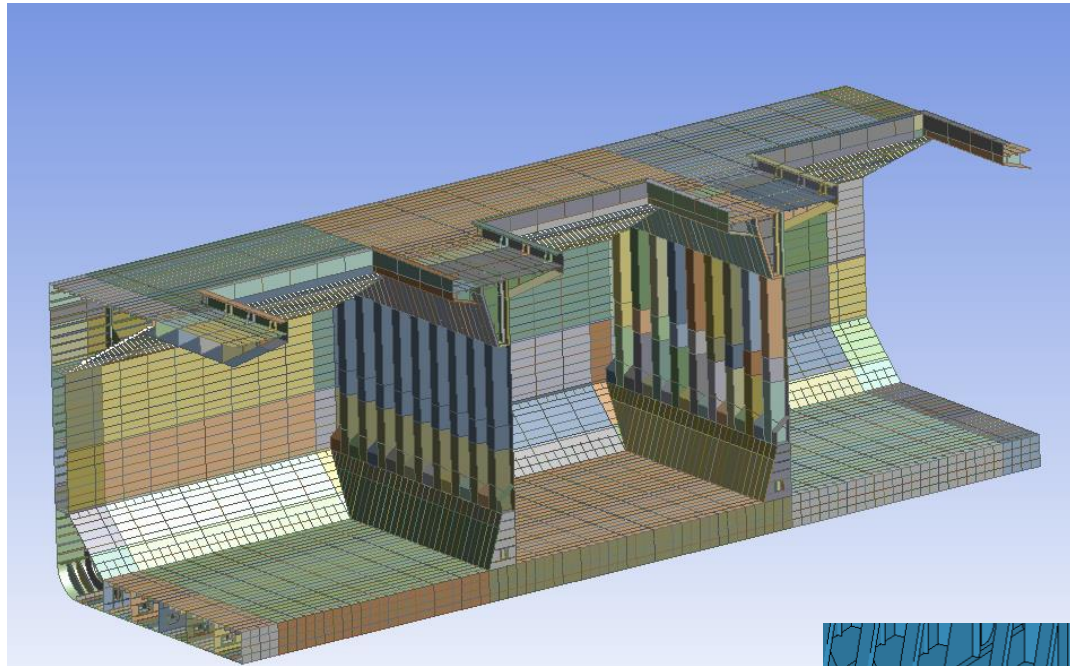


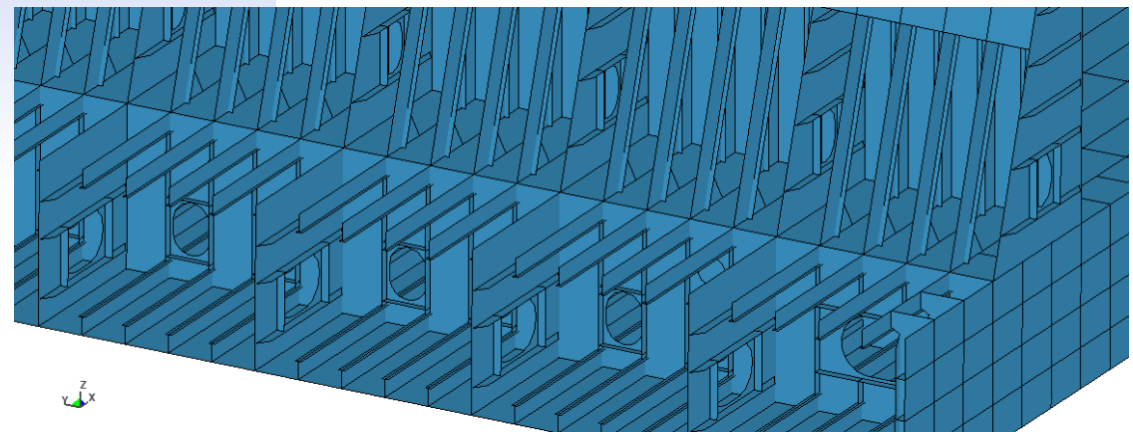
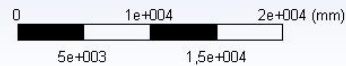
Fig. 3 Stress – strain curve

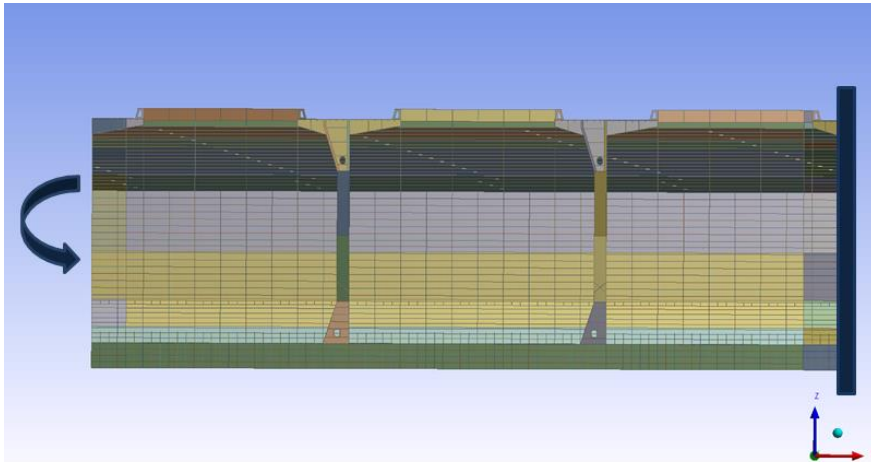
Bulk carrier – Finite element model



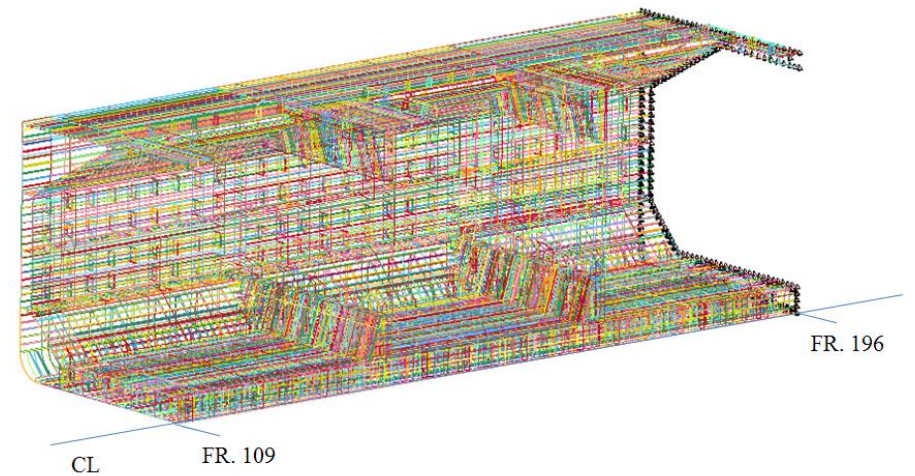
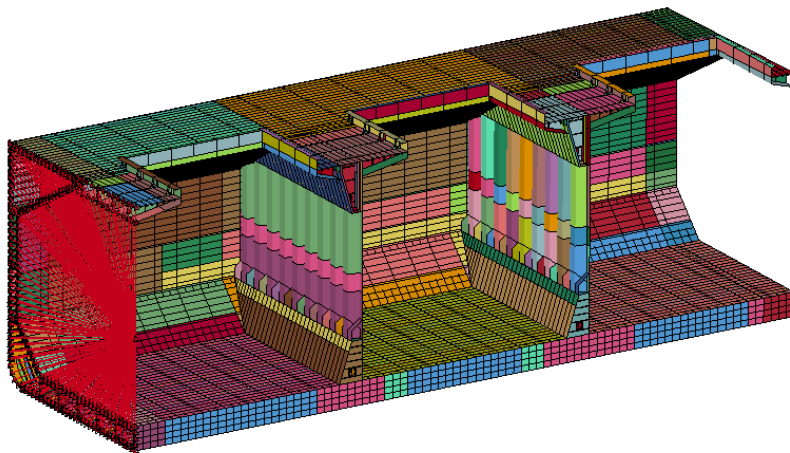
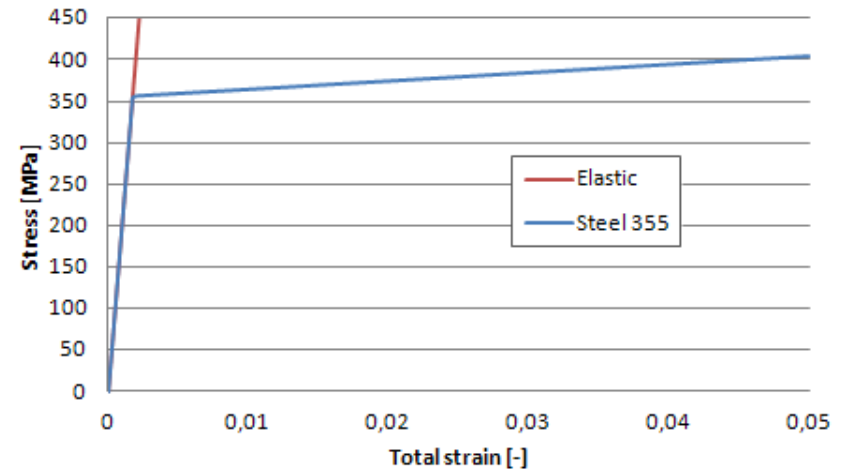
Build in Ansys Workbench

3 cargo holds, Fr.109 -196





Steel stress-strain curve

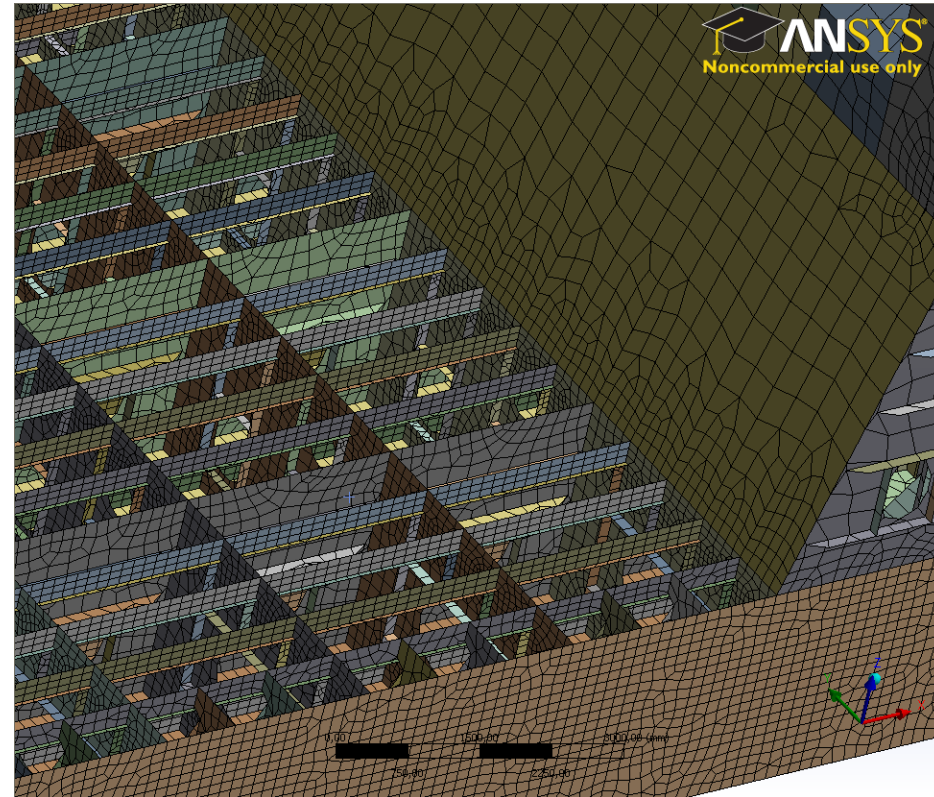
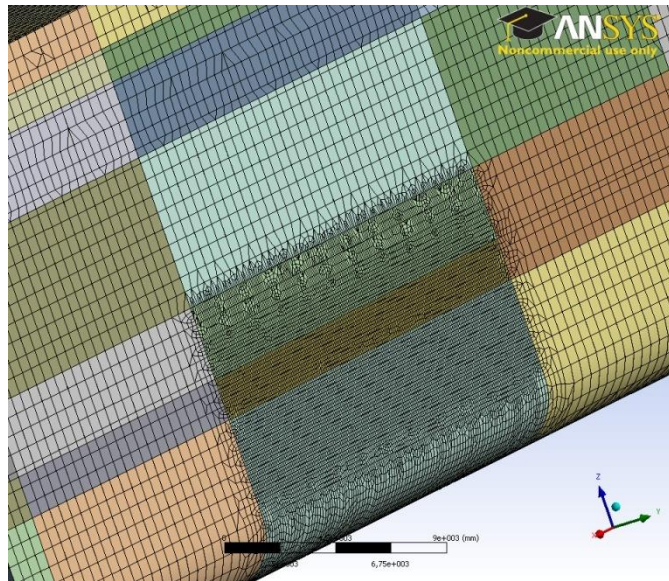


Mesh convergence

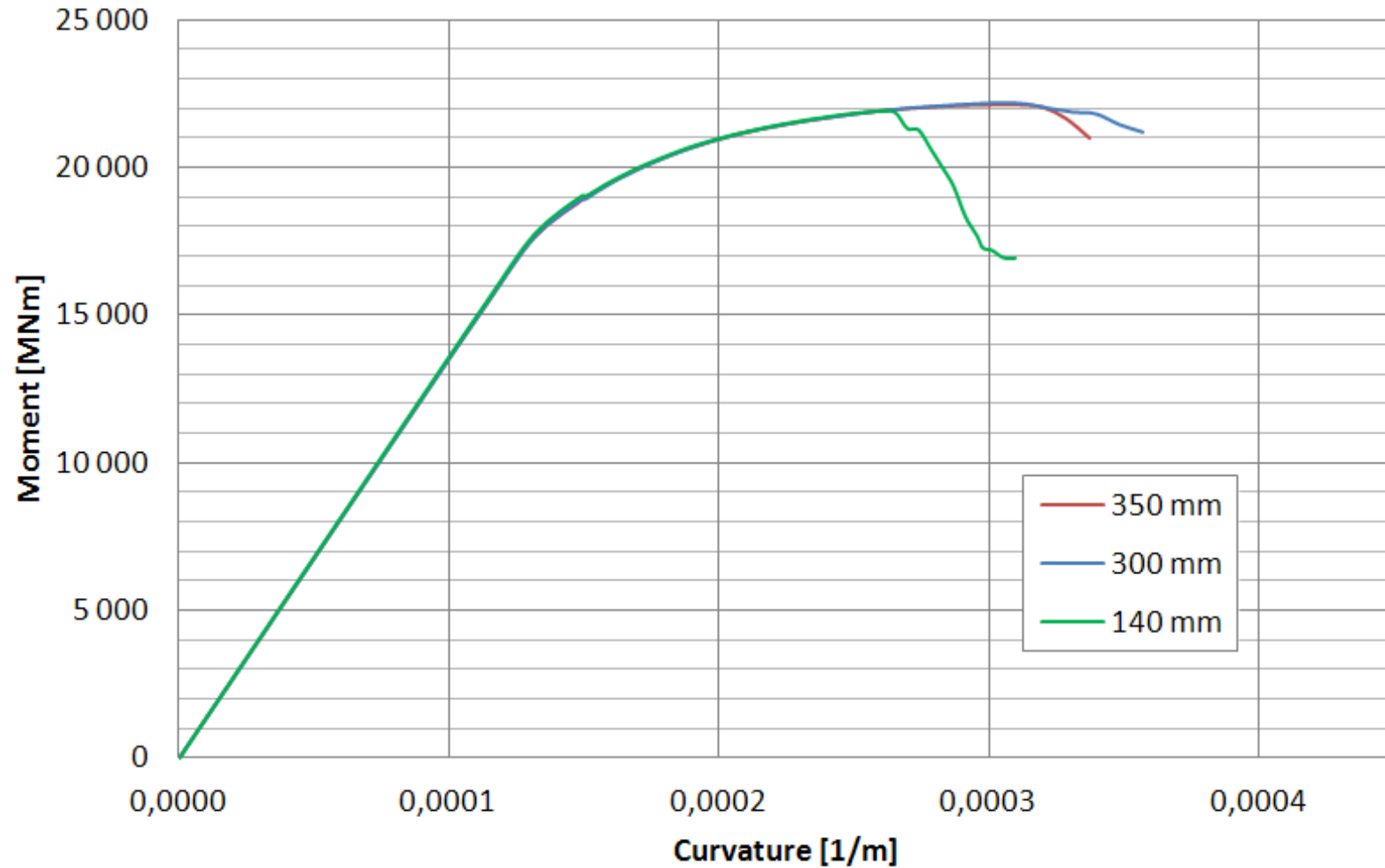
Mesh 1 – 350 mm

Mesh 2 – 300 mm

Mesh 3 – 140 mm

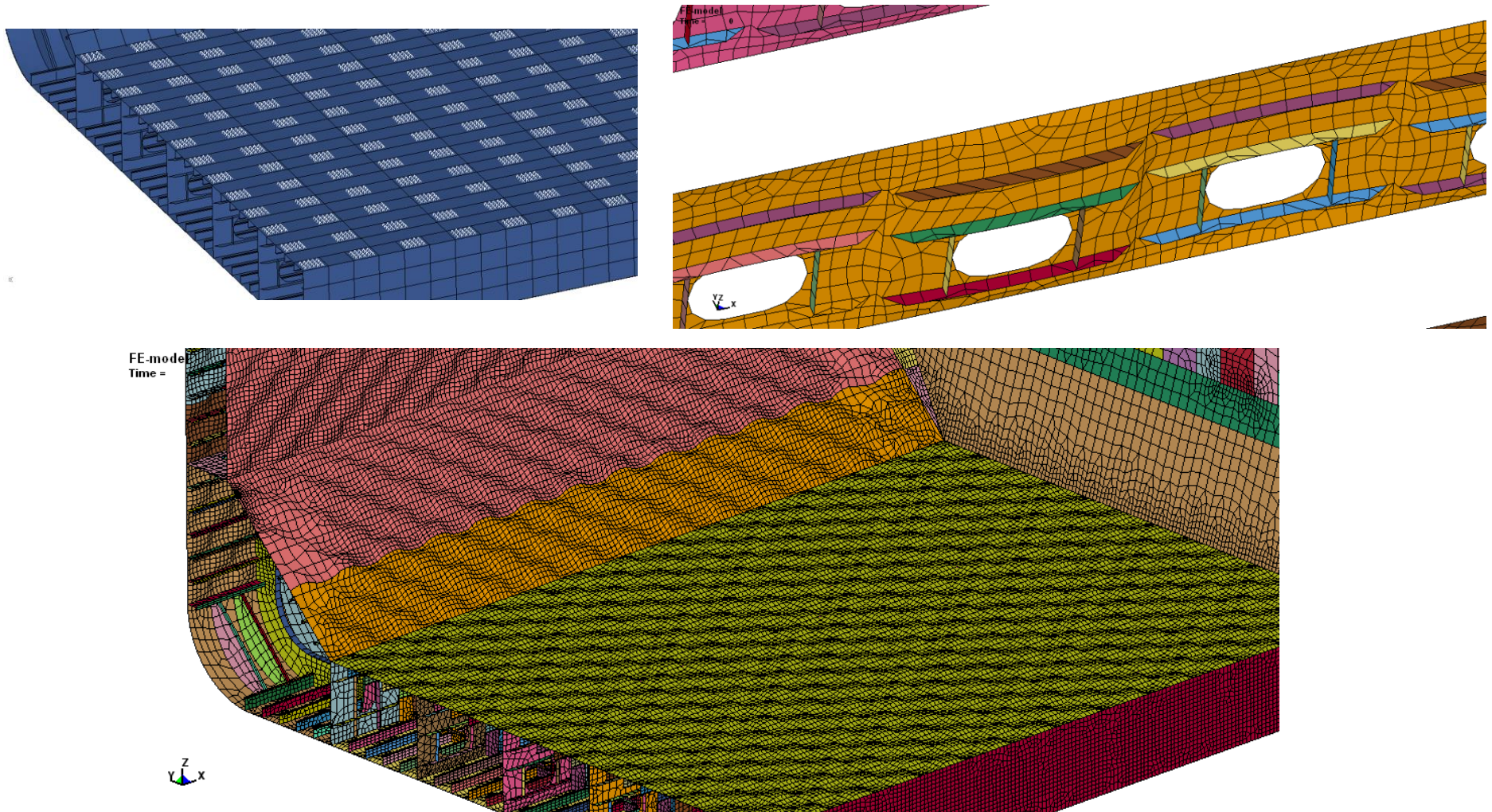


Ultimate strength

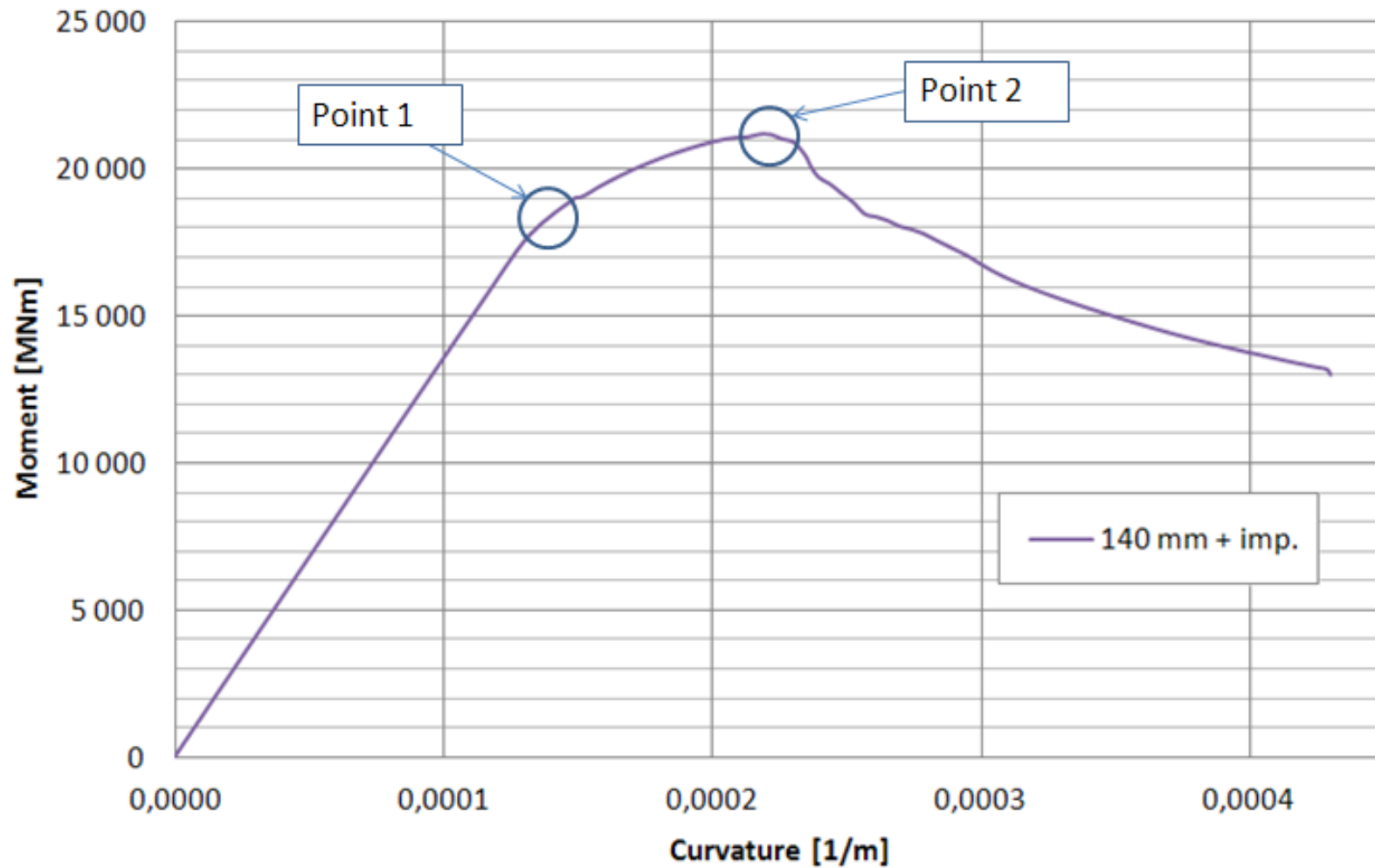


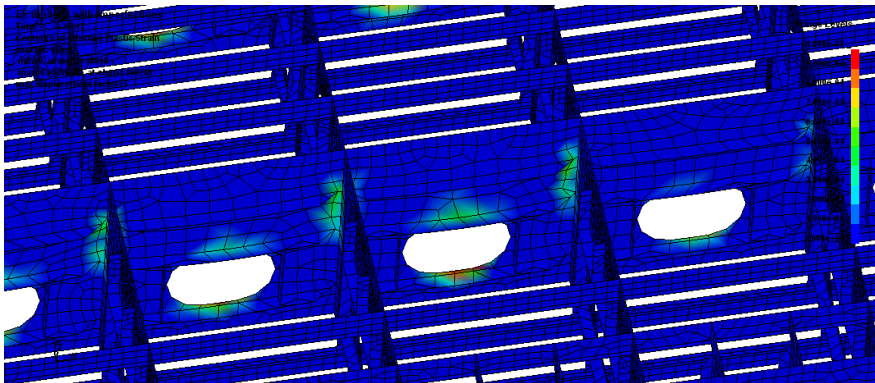
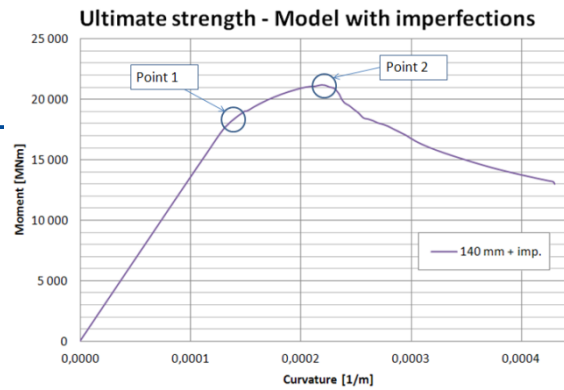
Imperfections

Around 3 mm for plating thickness 18,0 mm

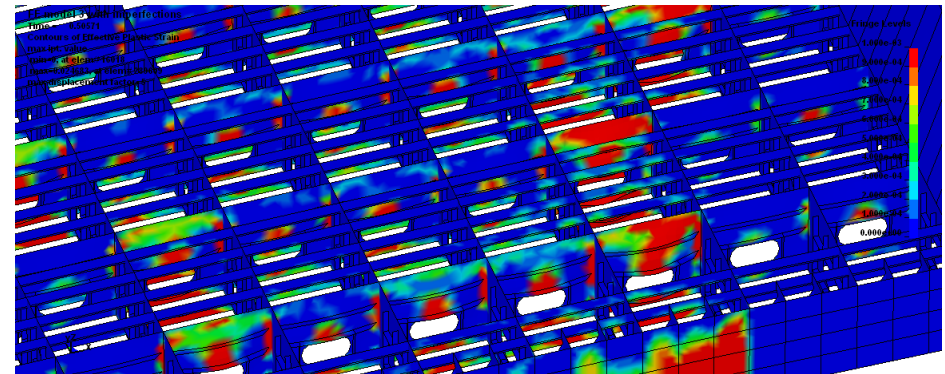


Ultimate strength – Model with imperfections

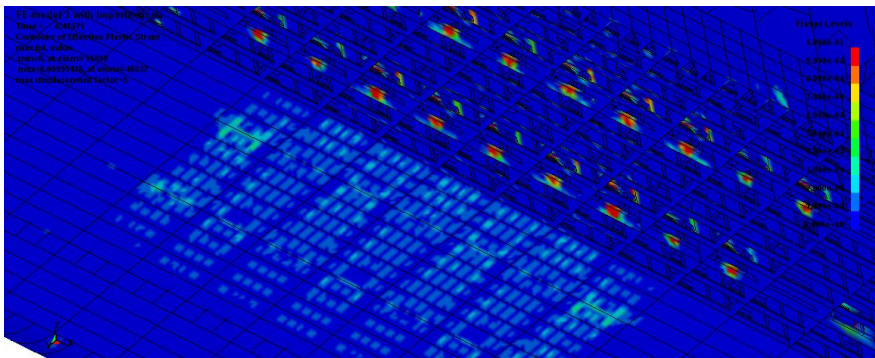




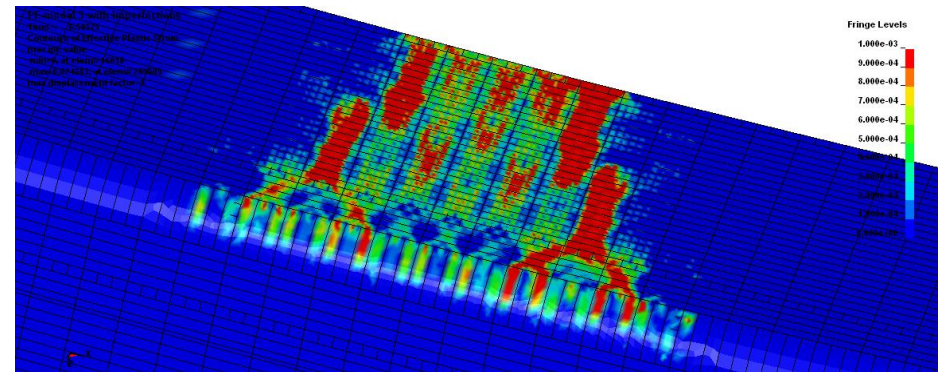
Plastic strain in girders for Point 1



Plastic strain in girders for Point 2

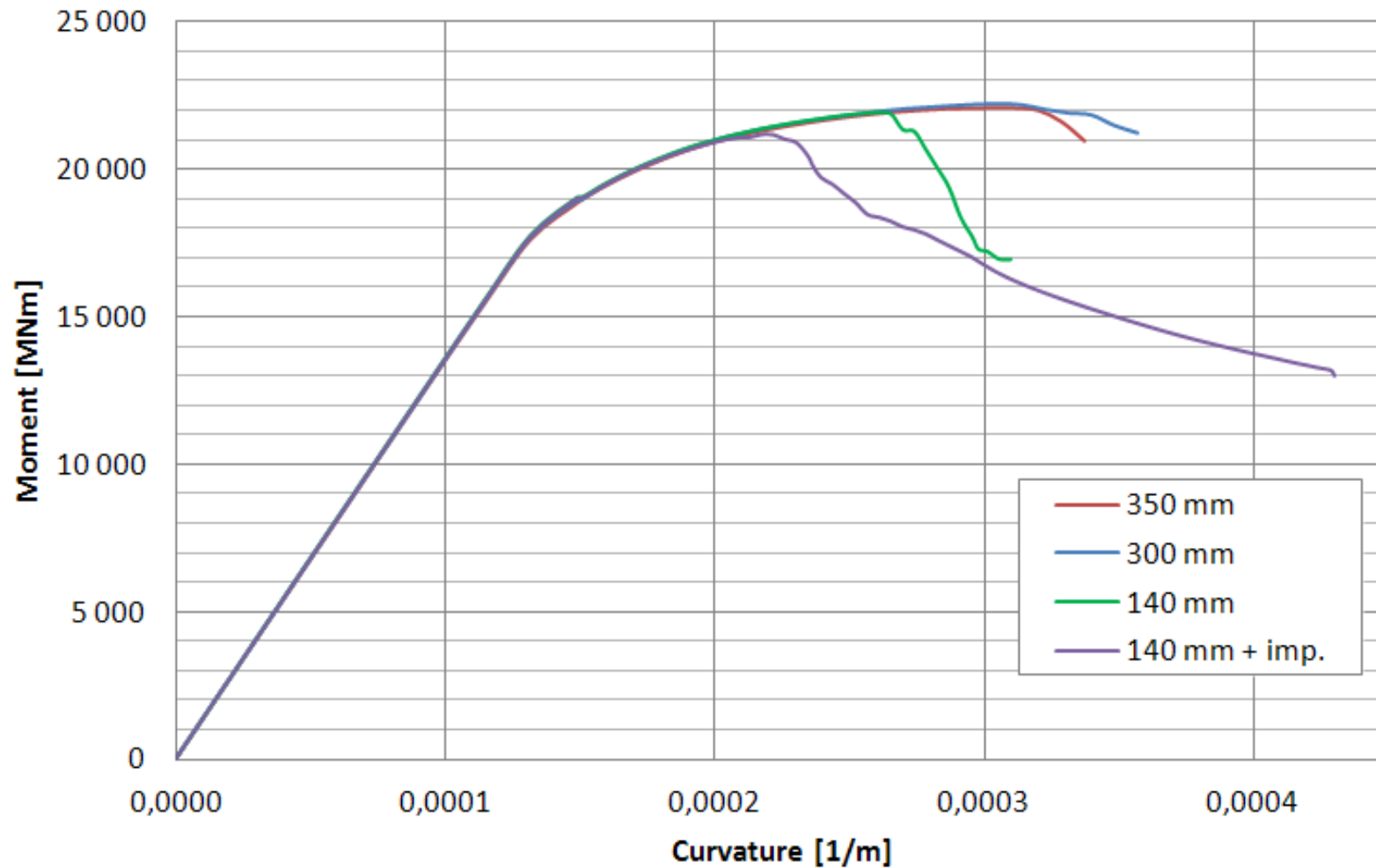


Plastic strain bottom plating after Point 1

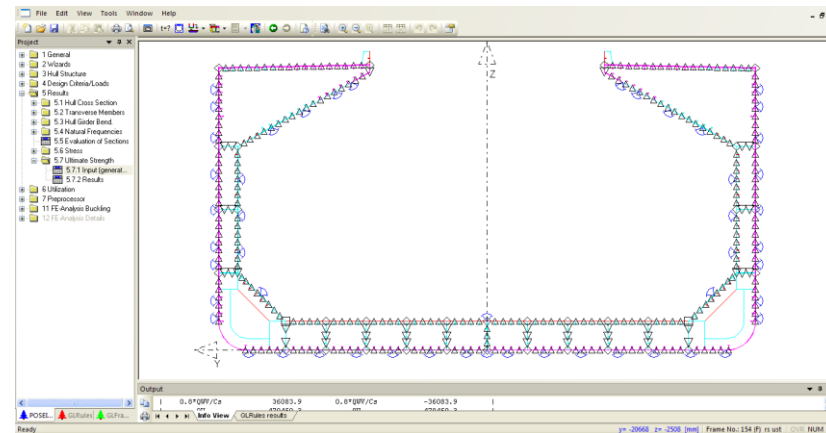
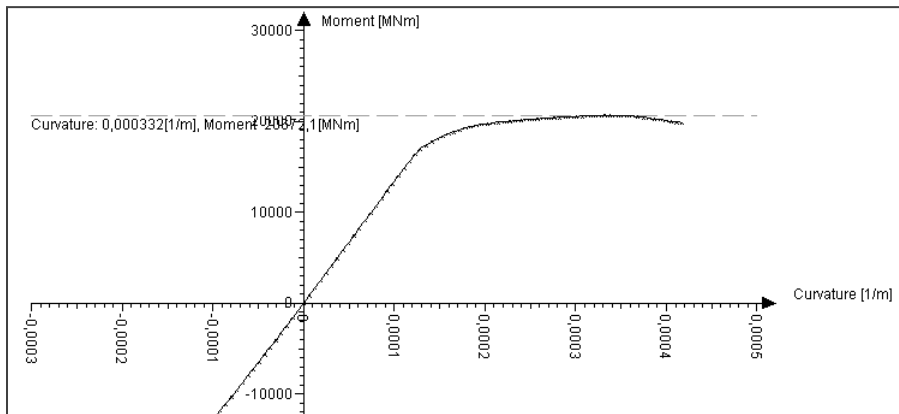
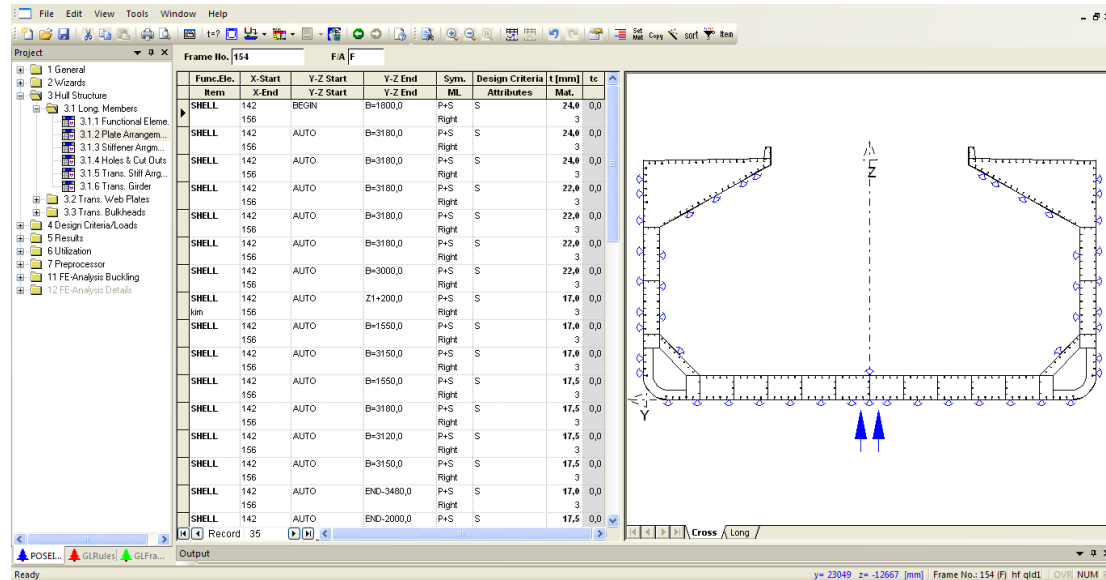


Plastic strain in bottom plating for Point 2

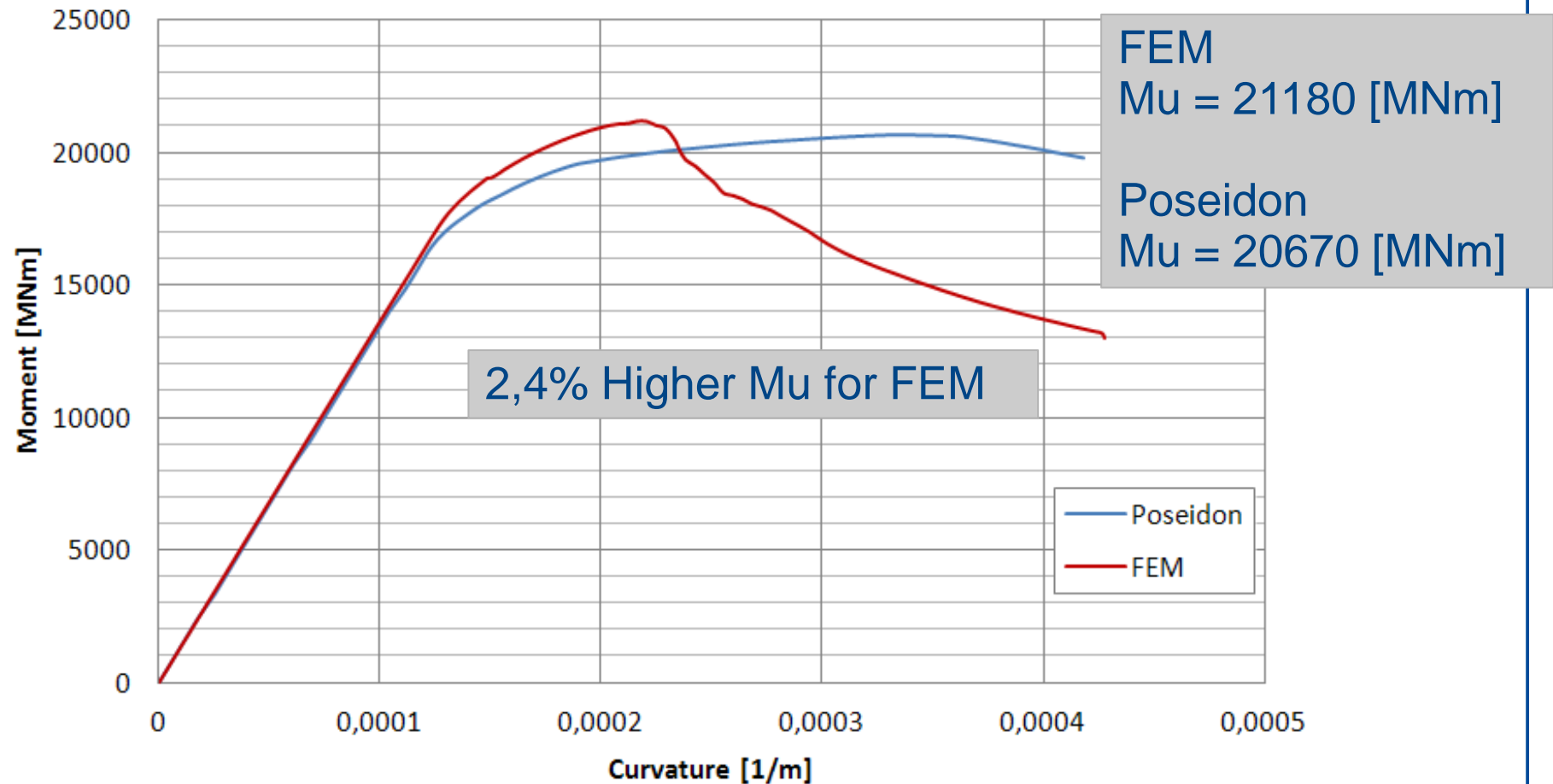
Ultimate strength



Bulk carrier - Poseidon model

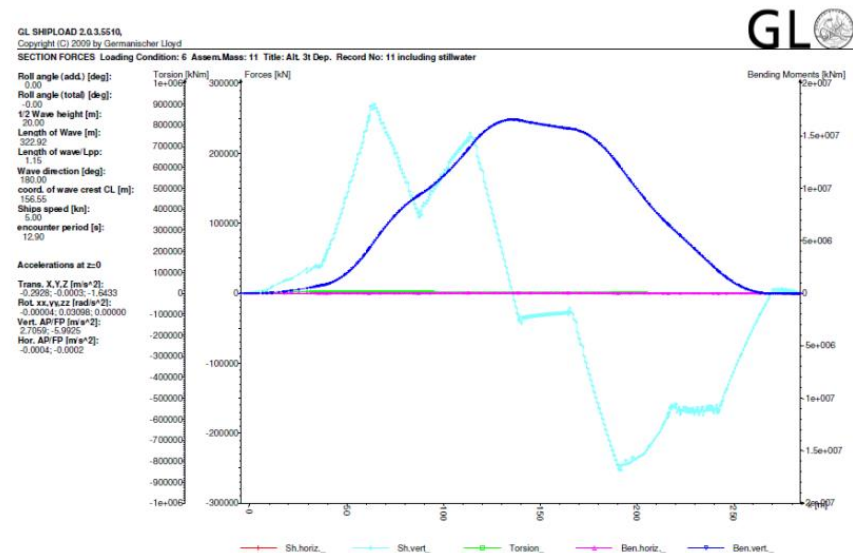
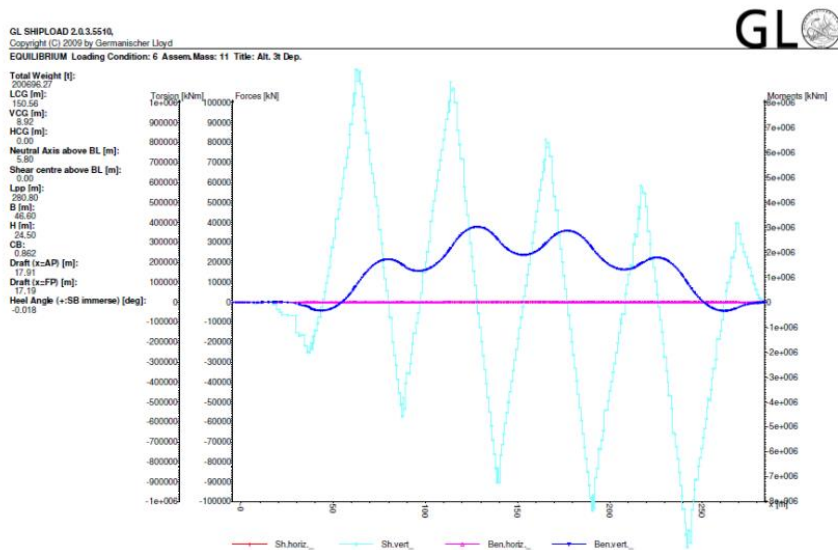


Ultimate strength

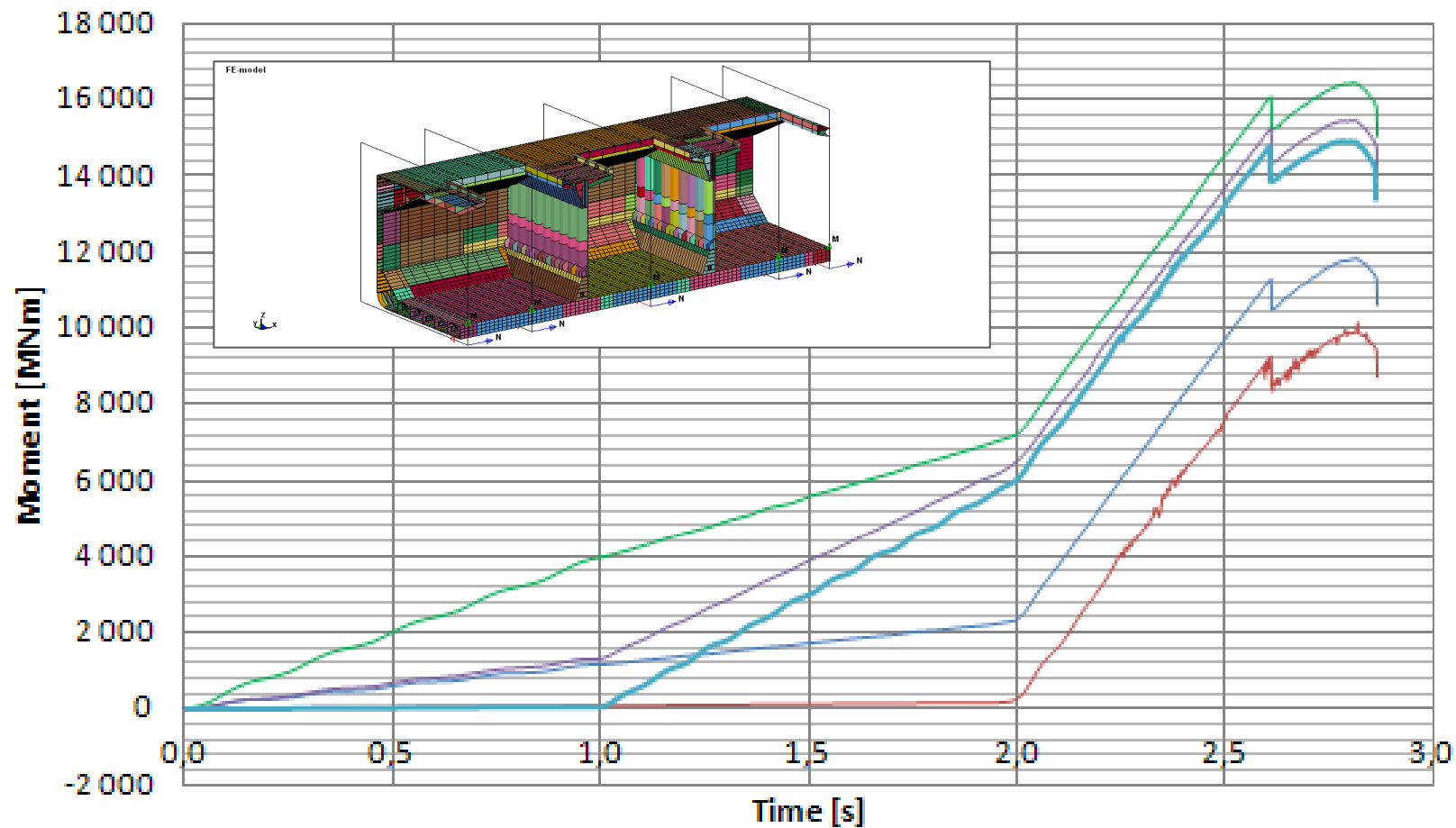


Local loads

- Load case 1: Wave height 13 meters,
- Load case 2: Wave height 15 meters,
- Load case 3: Wave height 20 meters,

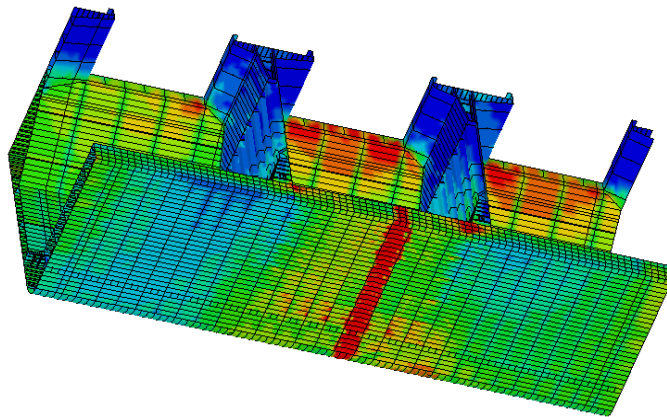


Ultimate strength 20 meters wave height



20 meters wave - results

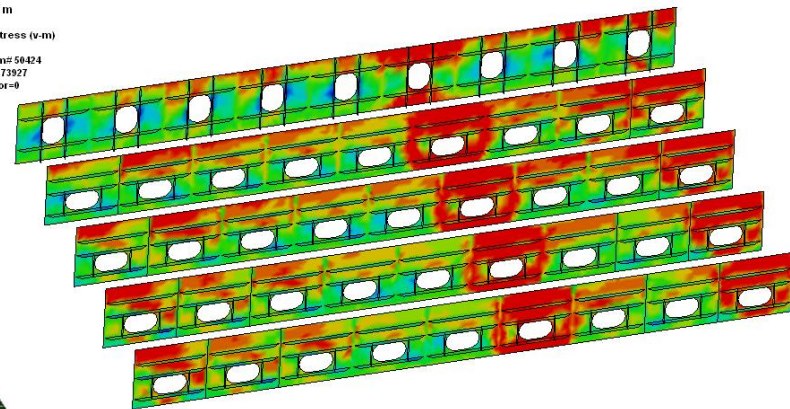
model 3 wave A 20 m
Time = 2.8604
Contours of Effective Stress (v-m)
max ipt. value
min=6.0796e-11, at elem= 50424
max=647.209, at elem= 73927



Fringe Levels
3.550e+02
3.195e+02
2.840e+02
2.485e+02
2.130e+02
1.775e+02
1.420e+02
1.065e+02
7.100e+01
3.550e+01
0.000e+00

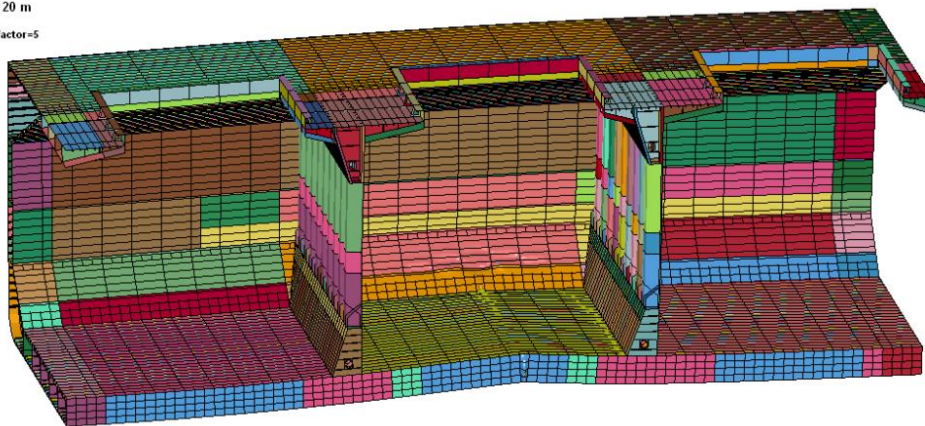


model 3 wave A 20 m
Time = 2.8604
Contours of Effective Stress (v-m)
max ipt. value
min=6.0796e-11, at elem= 50424
max=647.209, at elem= 73927
max displacement factor=0

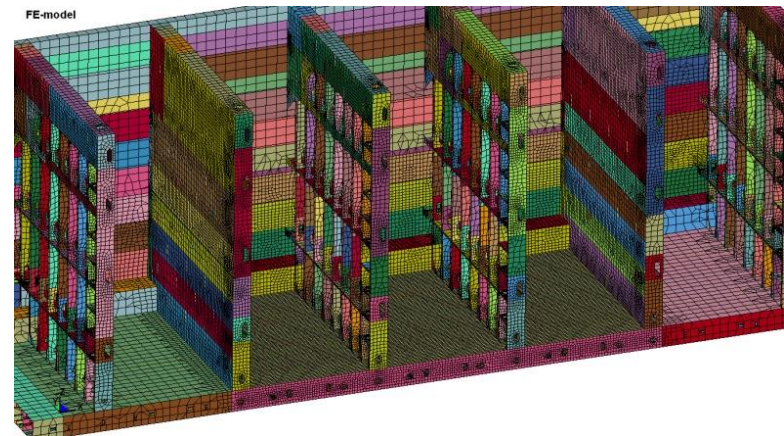
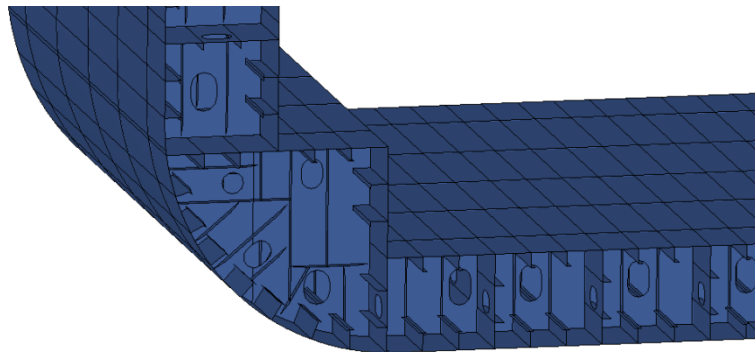
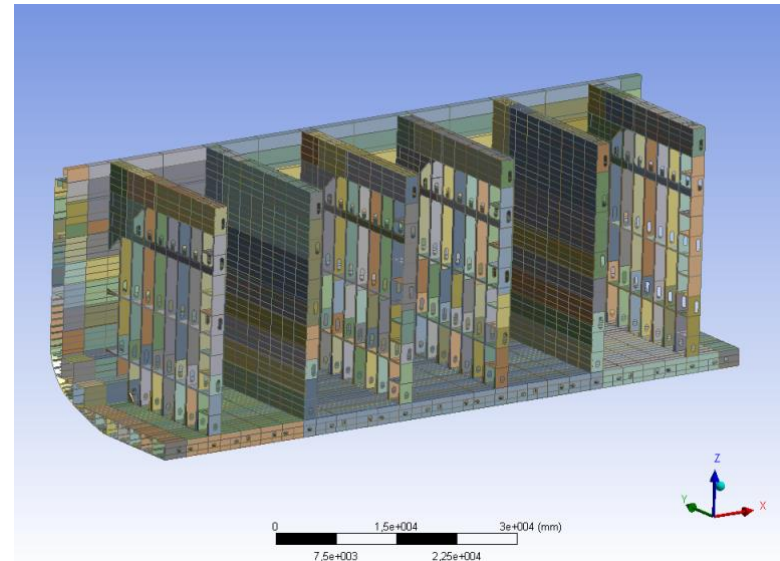
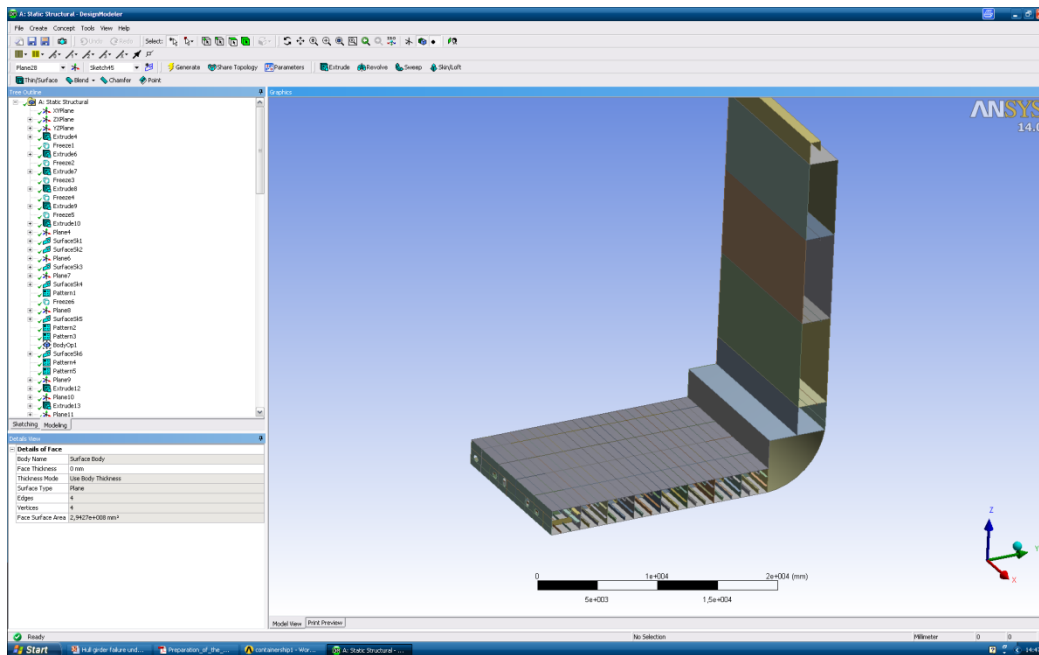


Fringe Levels
3.550e+02
3.195e+02
2.840e+02
2.485e+02
2.130e+02
1.775e+02
1.420e+02
1.065e+02
7.100e+01
3.550e+01
0.000e+00

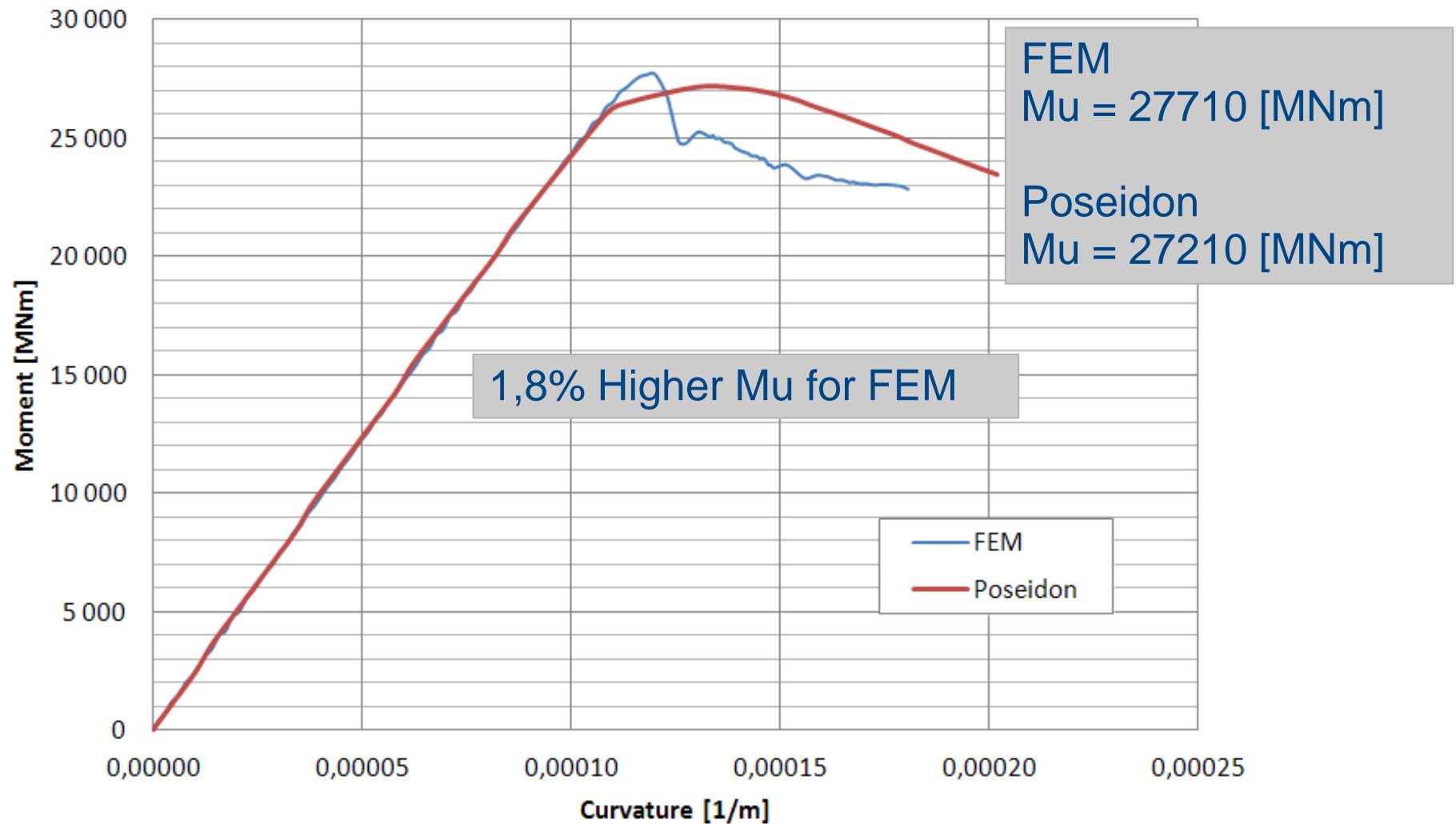
model 3 wave A 20 m
Time = 2.8604
max displacement factor=5



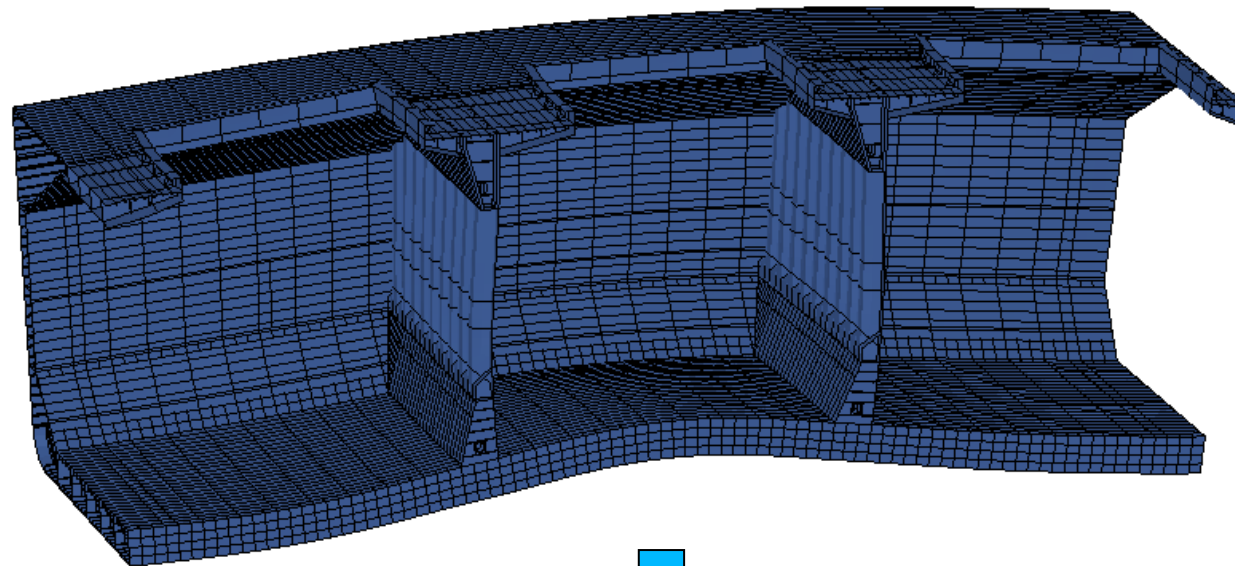
Initial container ship model



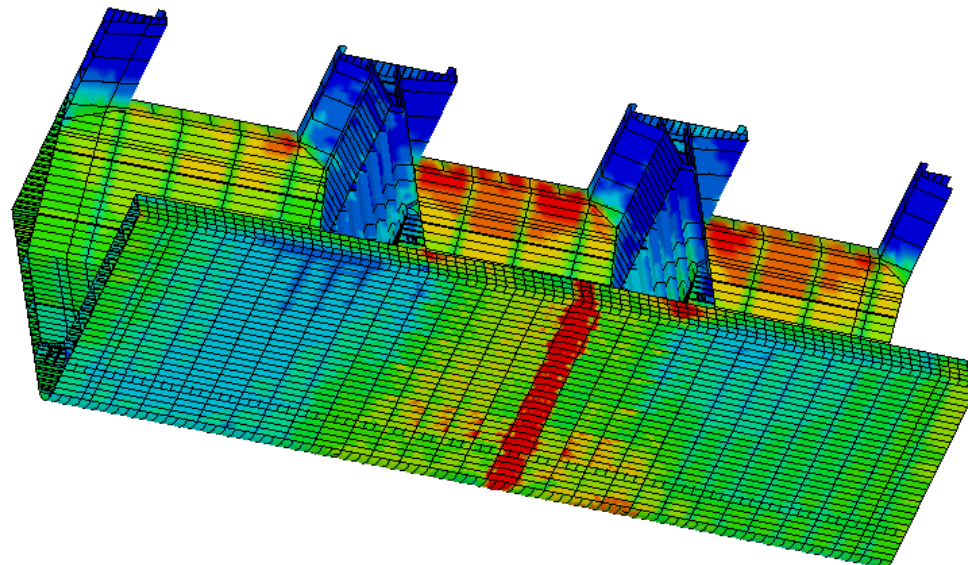
Ultimate strength



- ▶ Progressive collapse on two FE models were performed
- ▶ Smith's method and results from FEA are comparable
- ▶ Bottom bending effects decrease ship's ultimate strength



model 3 wave A 20 m
Time = 2.8604
Contours of Effective Stress (v-m)
max ipt. value
min=6.0796e-11, at elem# 50424
max=647.209, at elem# 73927



Fringe Levels

